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# *Use of high-energy X-ray microbeams for phase and strain mapping*

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***APS Users Meeting***

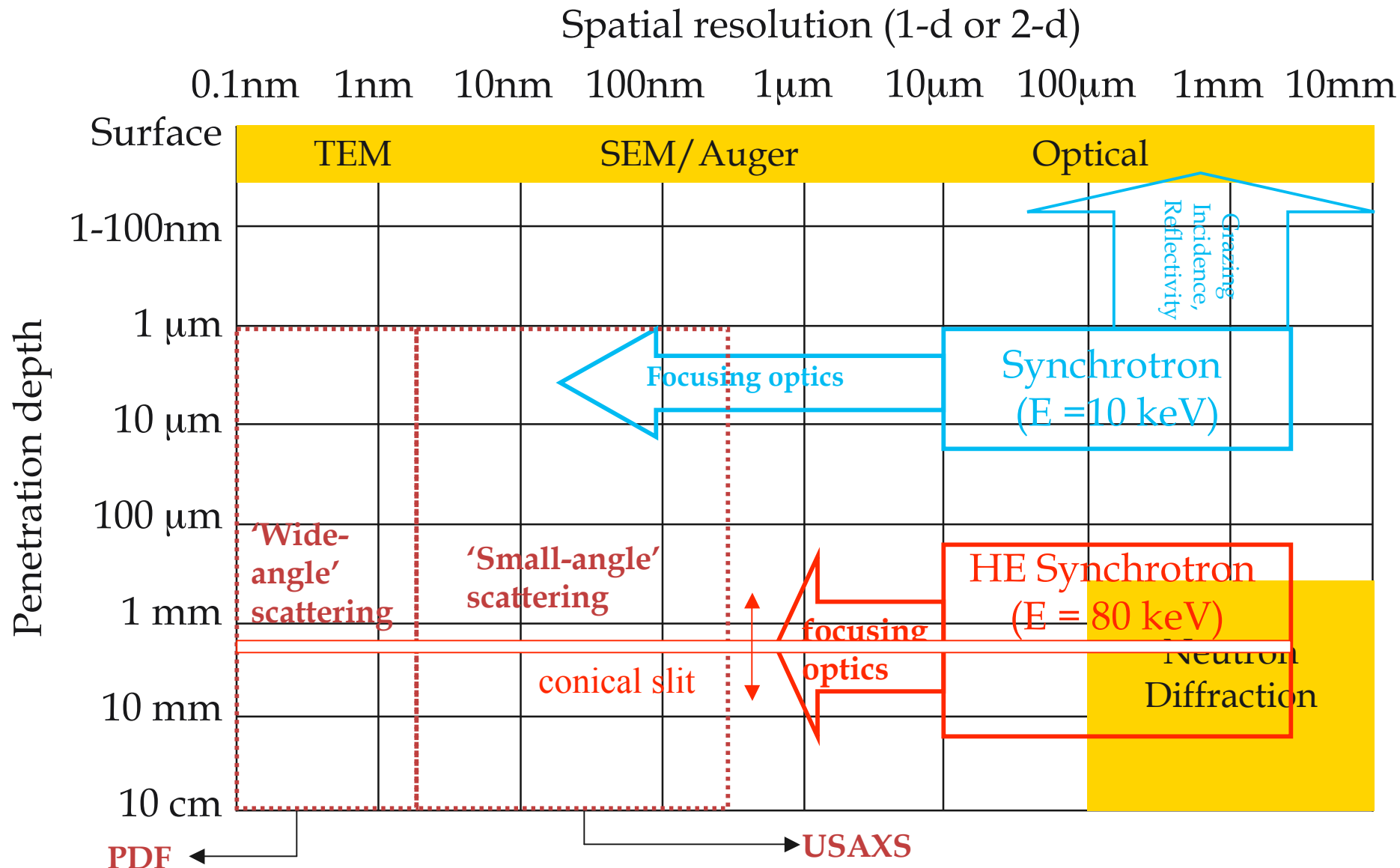
***May 9, 2007***

## Outline

- Survey of probe sizes & techniques
- Sector 1-ID beamline for high-energy x-ray studies
- Solid oxide fuel cell
  - Phase and strain mapping with 1-d resolution
- Advanced gear steel
  - Strain mapping with 3-d resolution

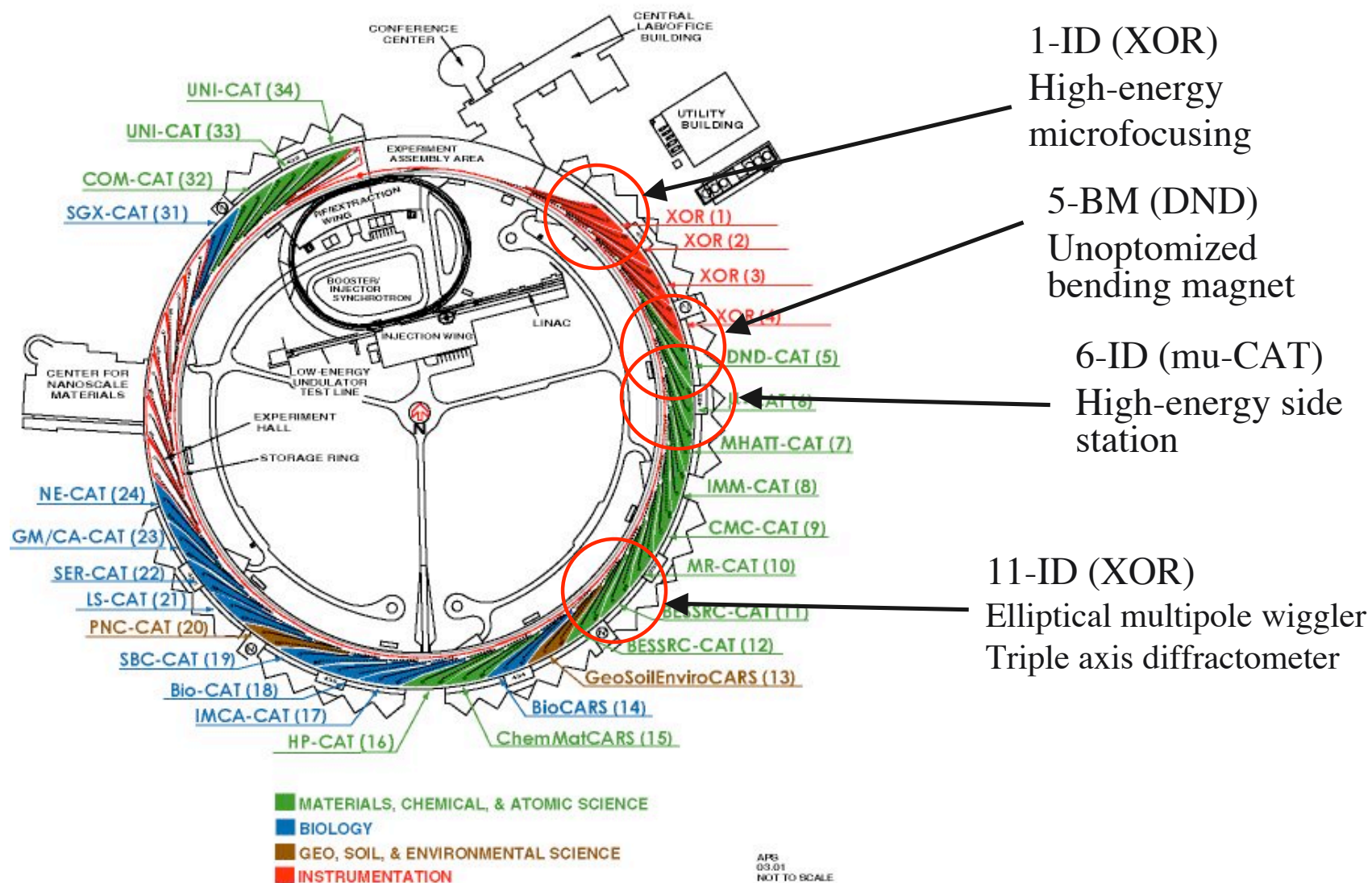


## Probe sizes of selected techniques

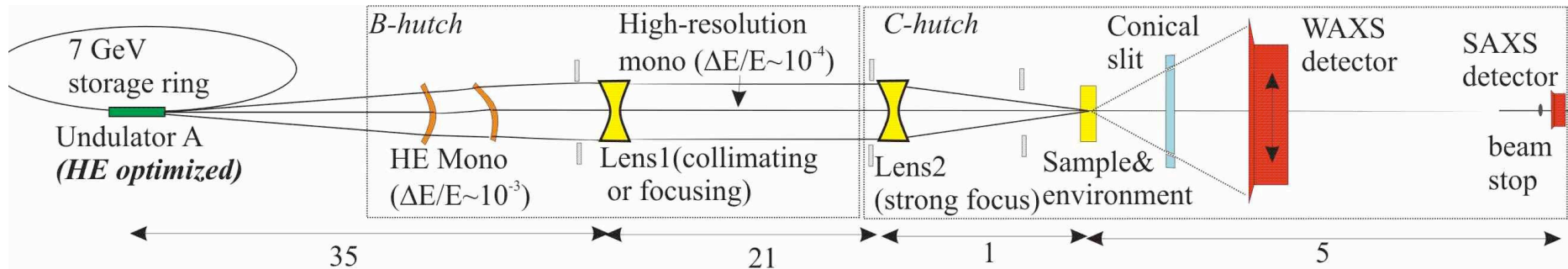


# Strain scanning at the APS

## APS Collaborative Access Teams by Sector & Discipline

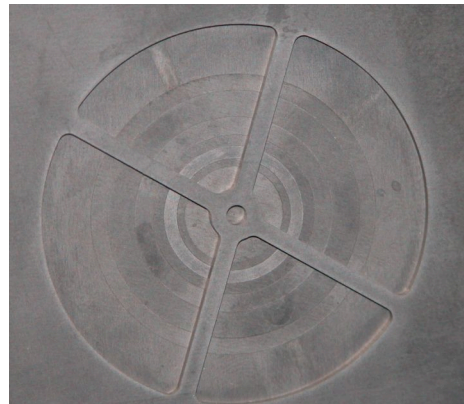


## APS 1-ID beamline

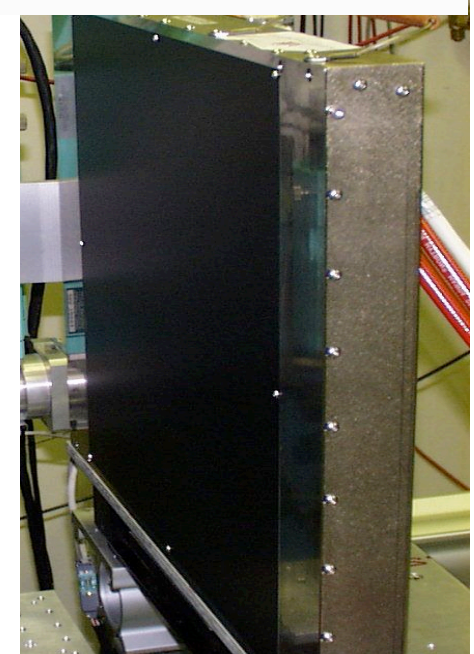


### Key components

- Undulator
- Optimized HE optics (transverse resolution)
- Environment
  - Furnaces
  - Tensile/compressive loading rigs
  - MTS device
- Conical slit for longitudinal resolution
- Large (fast) area detectors



Conical slit  
(7 rings)



GE detector



## Focusing using sawtooth refractive lenses

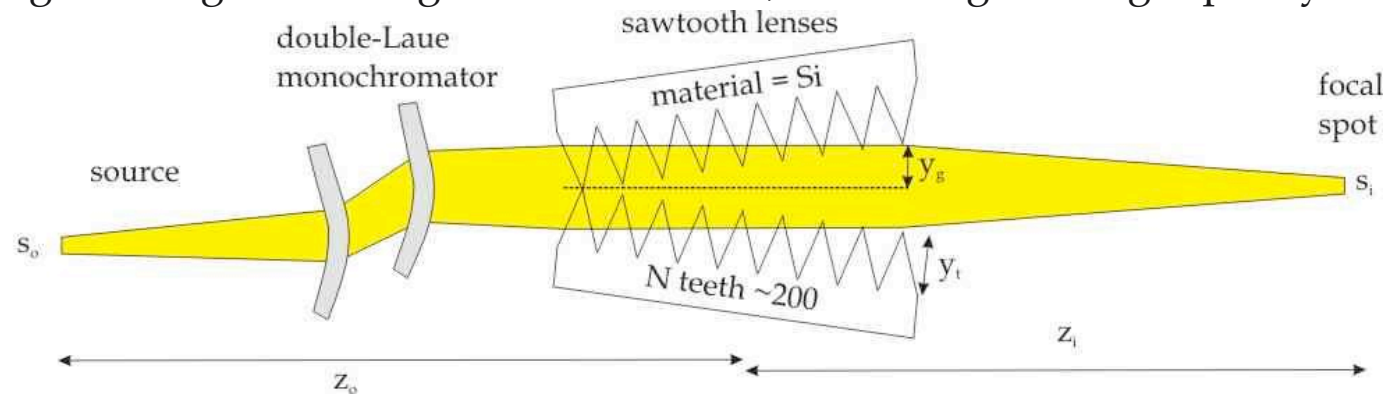
Collaborators: C. Ribbing (Uppsala) and B. Cederstrom (KTH), Sweden

Typical focal sizes:

18  $\mu\text{m}$  (weak focusing;  $z_o:z_i \sim 36:24 \text{ m}$ )

1.5  $\mu\text{m}$  (strong focusing;  $z_o:z_i \sim 60:1 \text{ m}$ )

Even at 'strong focusing' the divergence is  $\sim 200 \text{ urad}$ , low enough for high-quality diffraction



\* high-energy monochromator is effectively brilliance preserving - minimal aberrations (some dependence on bend radii)

\* use of pure material (single-crystal Si) gives minimal small-angle scattering from lens

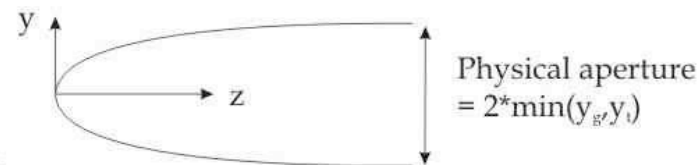
\* no absorption along lens optic axis ( $y=0$ )

\* lens focus distance  $z_i$  can be varied through  $y_g$

\* theoretical image size:

$$s_i = s_o(z_o/z_i)$$

canted sawtooth projection  $y(z)$  is effectively parabolic (aberrations typically submicron)



# ***Case study I: Phase and strain mapping in solid-oxide fuel cells***

*Collaborators:*

*Di-Jia Liu and Terry Cruze*

*Chemical Technology Division, ANL*

# Electrochemical Processes for Solid Oxide Fuel Cells (SOFCs)

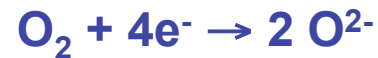
## Operating Principle of an SOFC

### Anode



**H<sub>2</sub> & CO Oxidation Reactions**

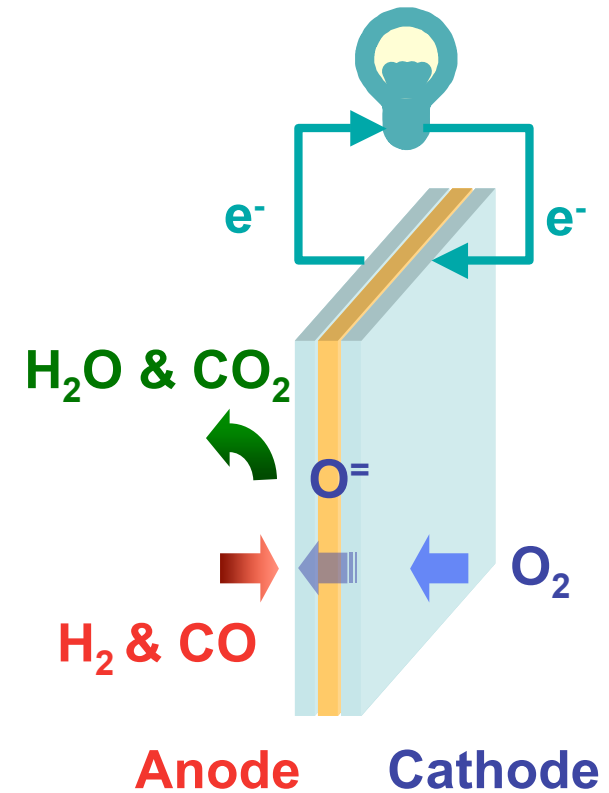
### Cathode



**O<sub>2</sub> Reduction Reaction**

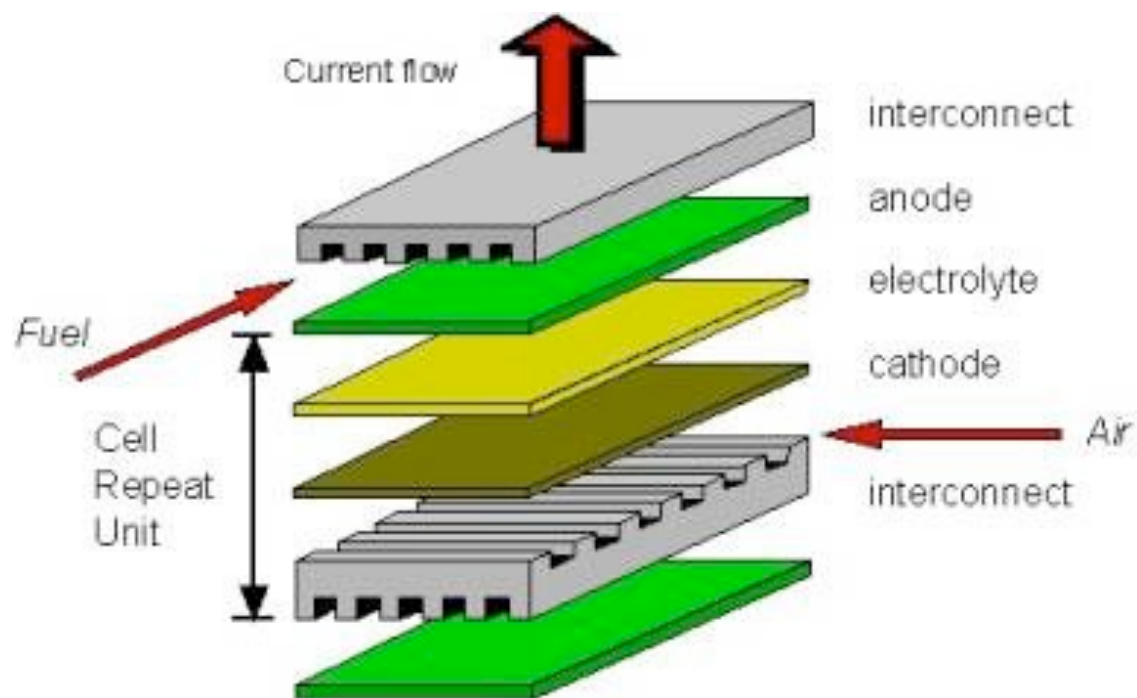


Artist's rendition of FutureGen power plant



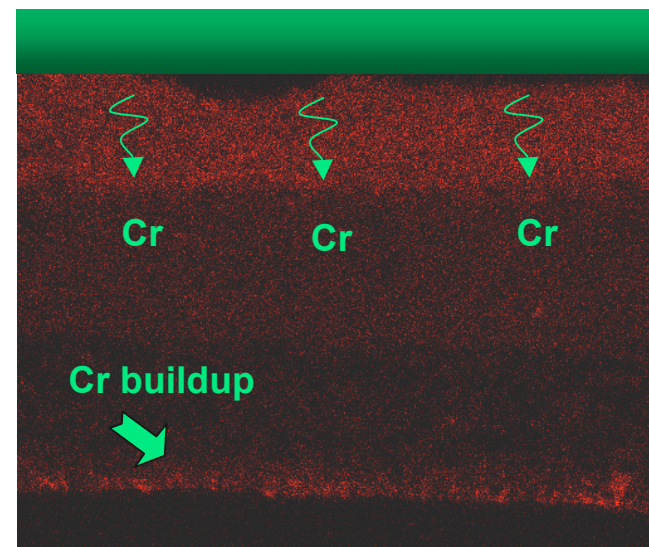


## ***Metallic Interconnect is Crucial in Reducing Material & Manufacturing Cost for SOFC***



# Cr Poisoning – A Material Challenge in SOFC Development

- SOFC deactivation is often associated with Cr accumulation in the cathode originated from metallic interconnect
- Knowledge of different Cr species & distribution is critical for understanding the deactivation mechanism
- Past experiments were limited to imaging (SEM, EDX, etc.) inconclusive in separating phase & distribution
- Conventional XRD method lacks spatial resolution and sensitivity



Cr Ka1

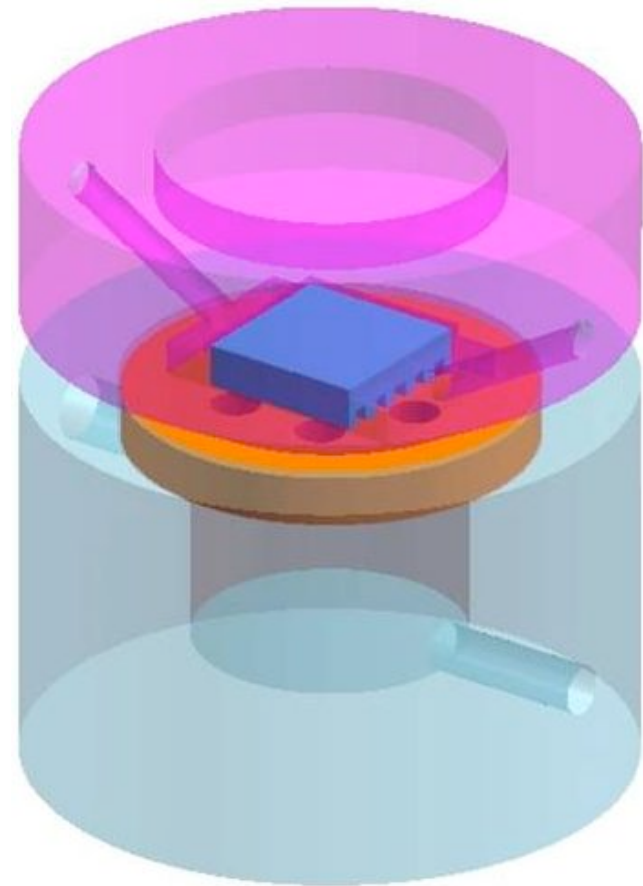
**Significant enrichment of Cr is observed at the cathode and electrolyte interface**

**Use microfocused high-energy x-rays to map Cr phases, internal strains and phase stoichiometry**

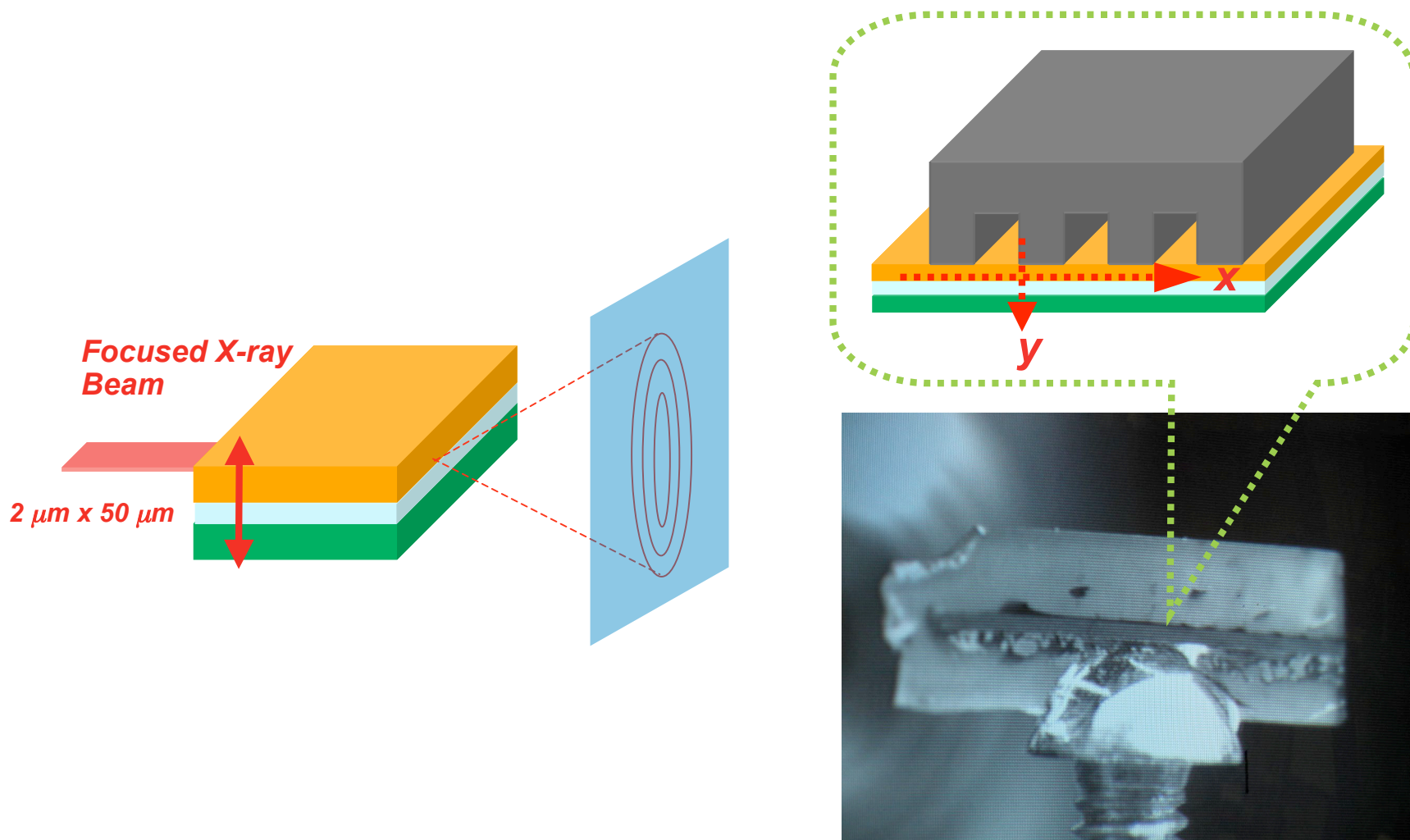
# *Button Cell Setup for Cr Poisoning Study*

## Test Conditions

- Current Density 250 mA/cm<sup>2</sup>
- Air Flow 70 sccm
  - (at -1.15A, ~25% O<sub>2</sub> utilization)
- Fuel Flow 400 sccm (50% N<sub>2</sub>, 50% H<sub>2</sub>)
  - (at -1.15A, ~4% H<sub>2</sub> utilization)



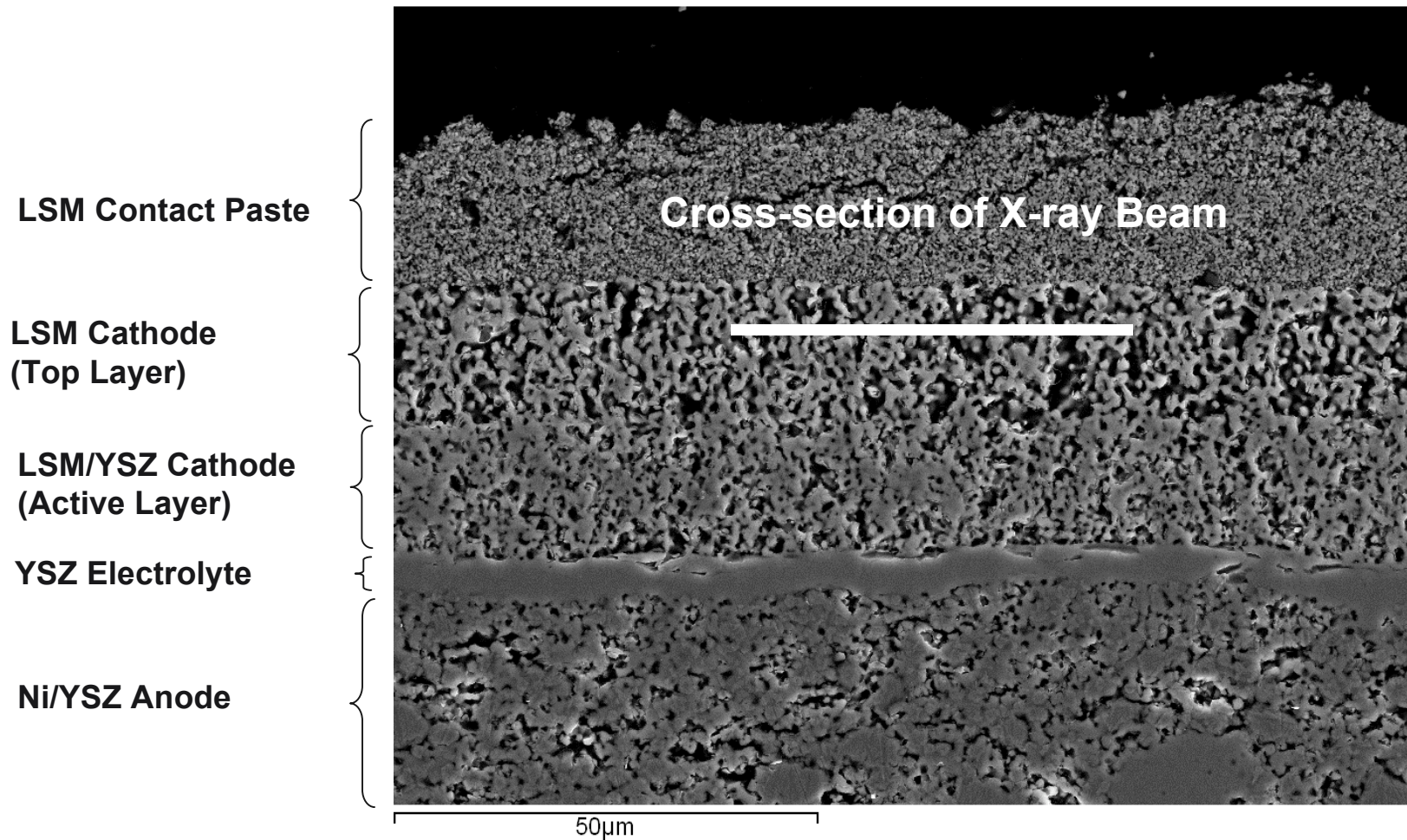
# HEWAXS Characterization of Chromium Phase and Spatial Distributions in a Contaminated SOFC



Cross-sectioned SOFC embedded in epoxy

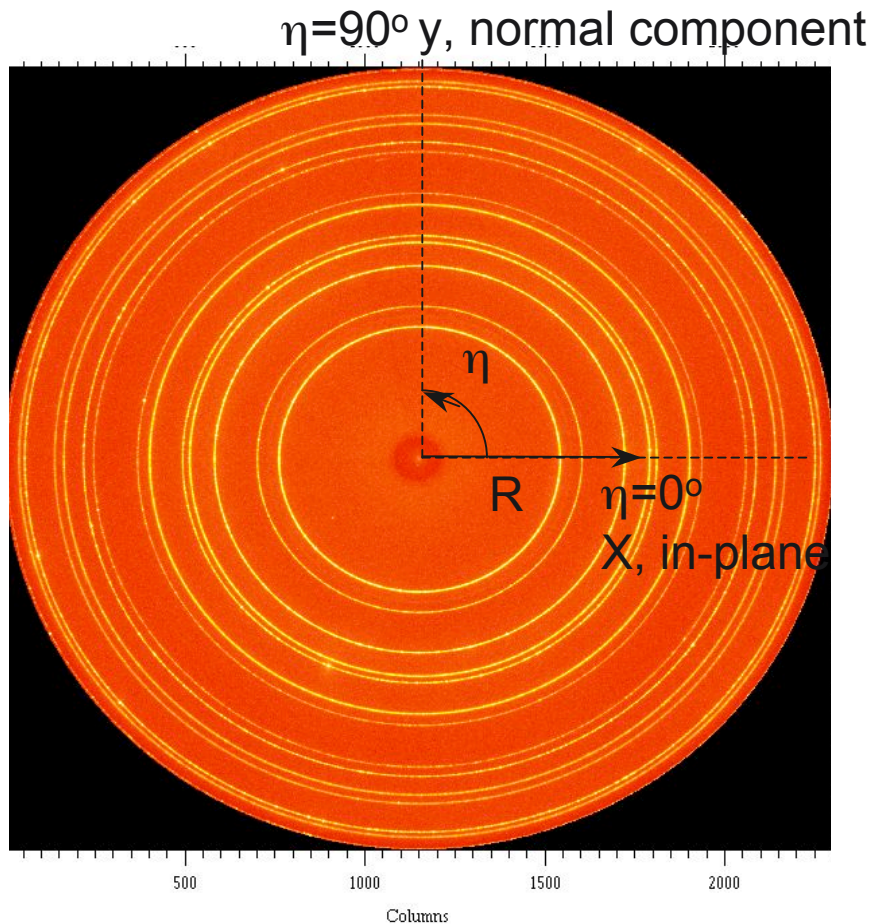


## Cross-section of SOFC Investigated (1mm thick)



SEM Image of InDec SOFC Cross-section

## Diffraction data from SOFC



**Typical pattern**  
**Mar345, E=80.7 keV**

### Intensity

- Smooth & constant vs azimuth (fine grained, no texture)
- Phase composition analysis

### Radius versus azimuth

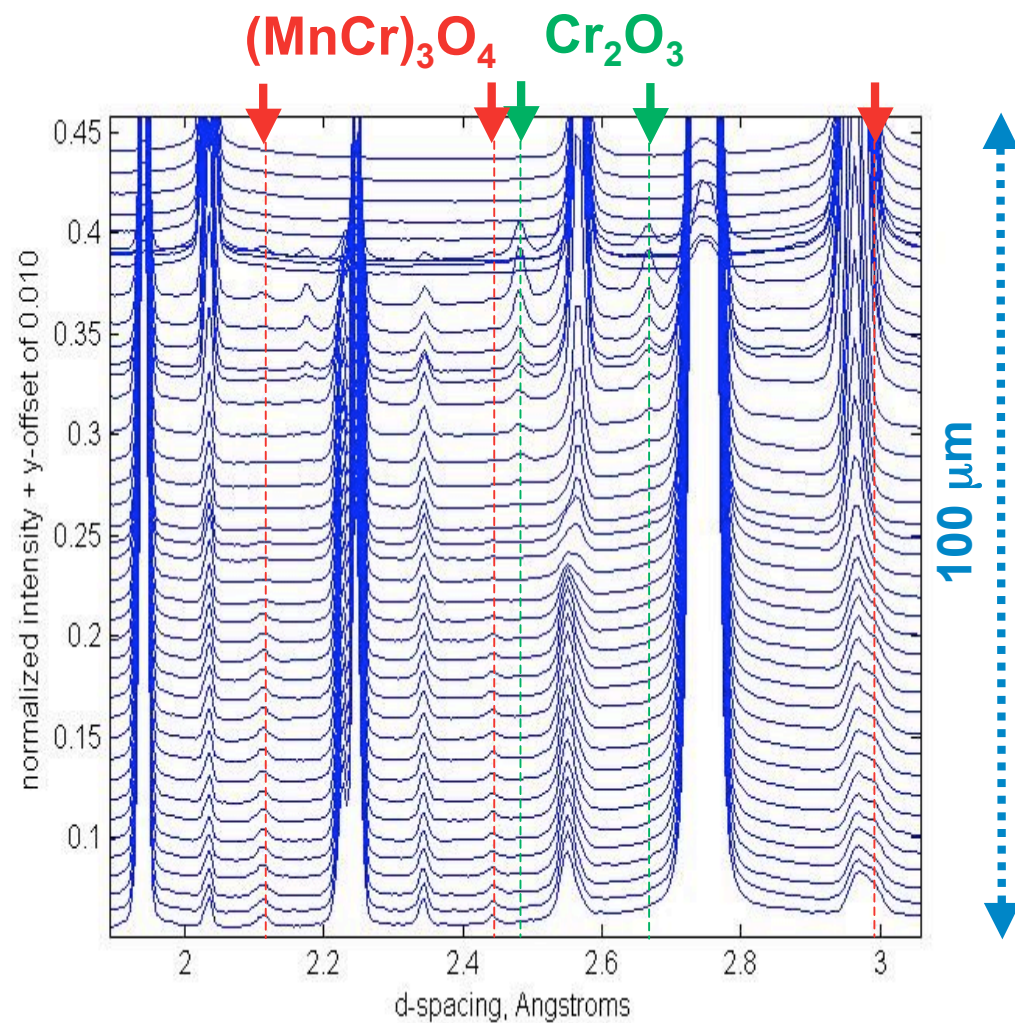
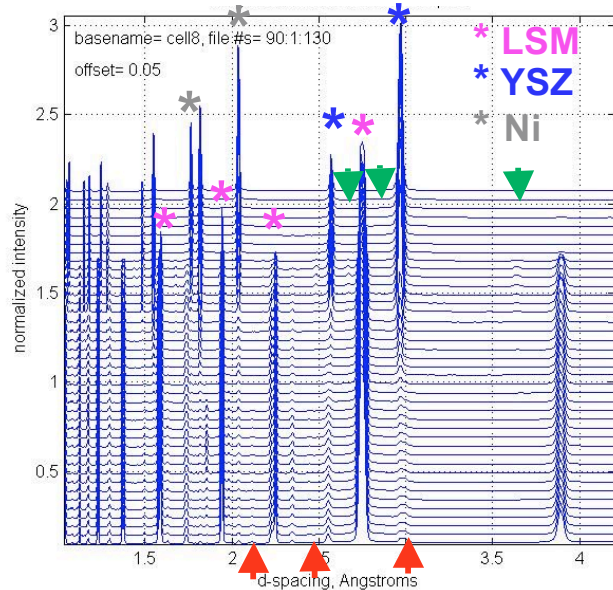
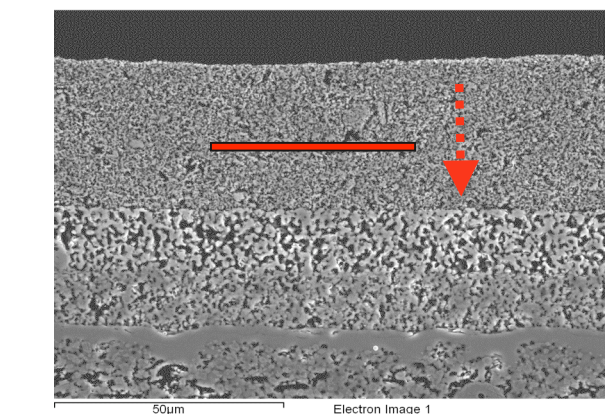
- deviatoric strain
- $\Delta\epsilon = - (r_{xx} - r_{yy})/r_{mean}$

### Mean radius

- Estimate intraphase composition changes
- $\Delta d_{hkl}/d_{hkl} = - (r_{hkl} - r_{mean})/r_{mean}$

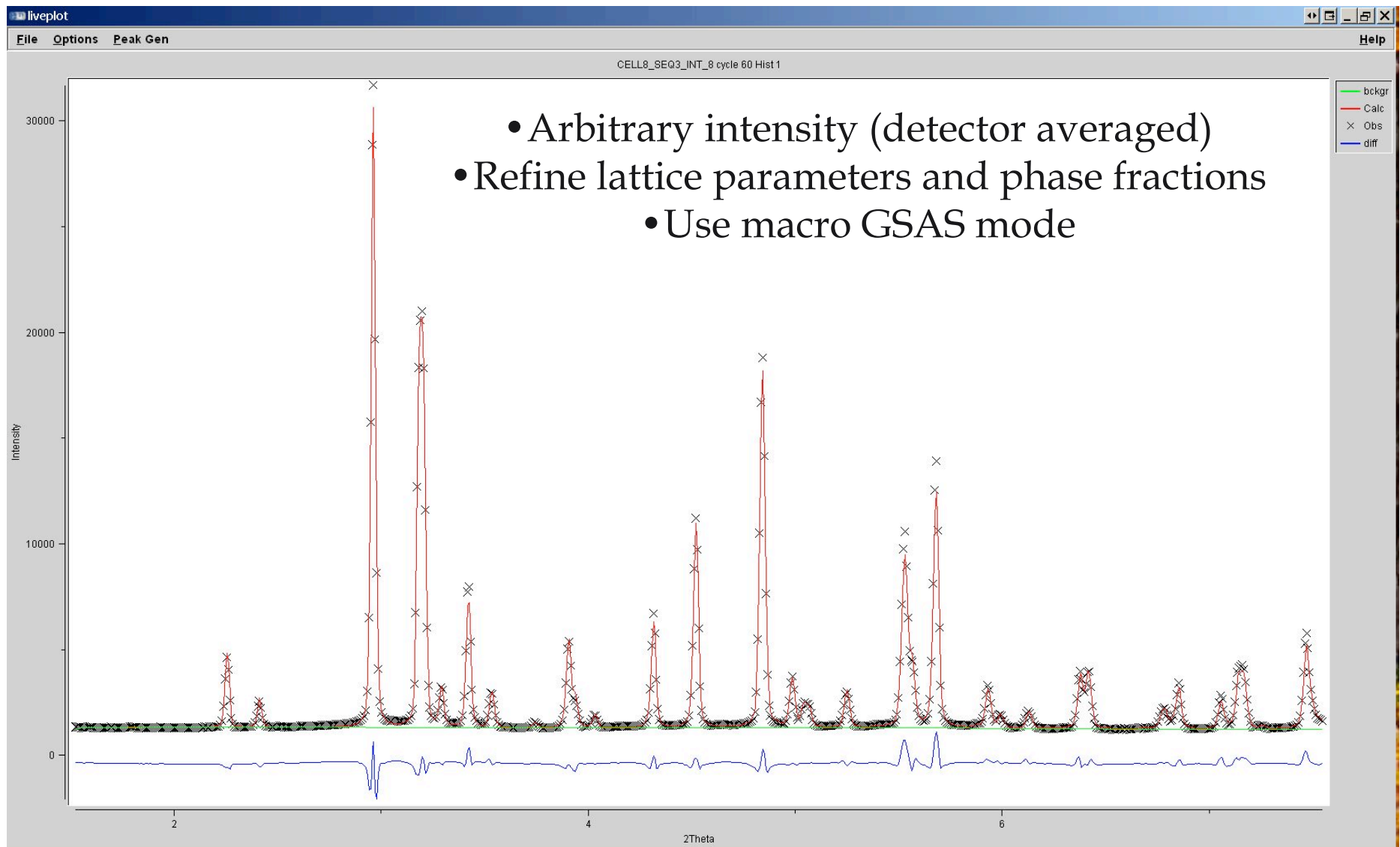


# Chromia and Manganese Chromium Spinel are Unambiguously Identified

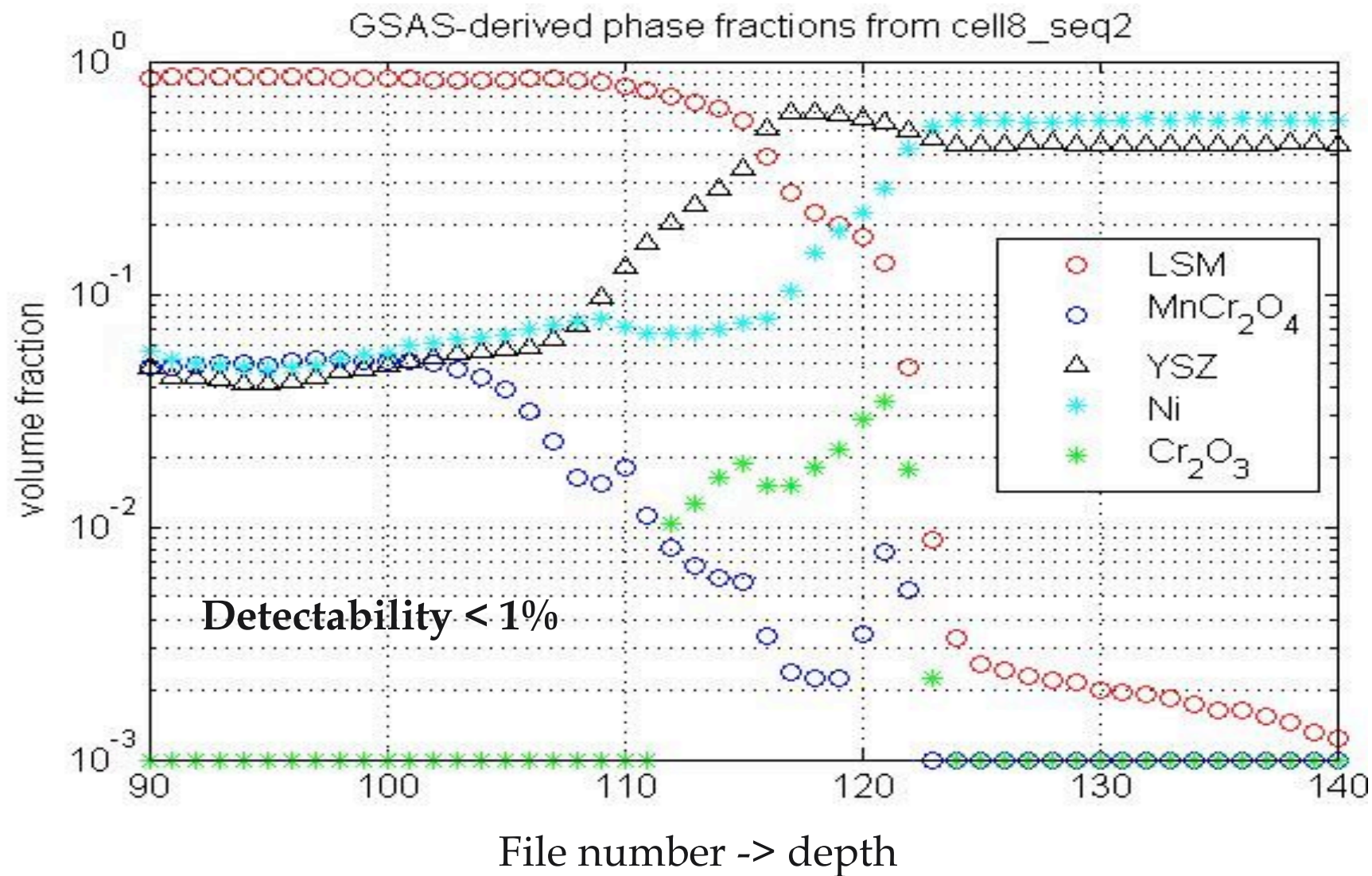


**Vertical Scan thru Cathode Depth**

## GSAS refinement – interface region (5 phases)



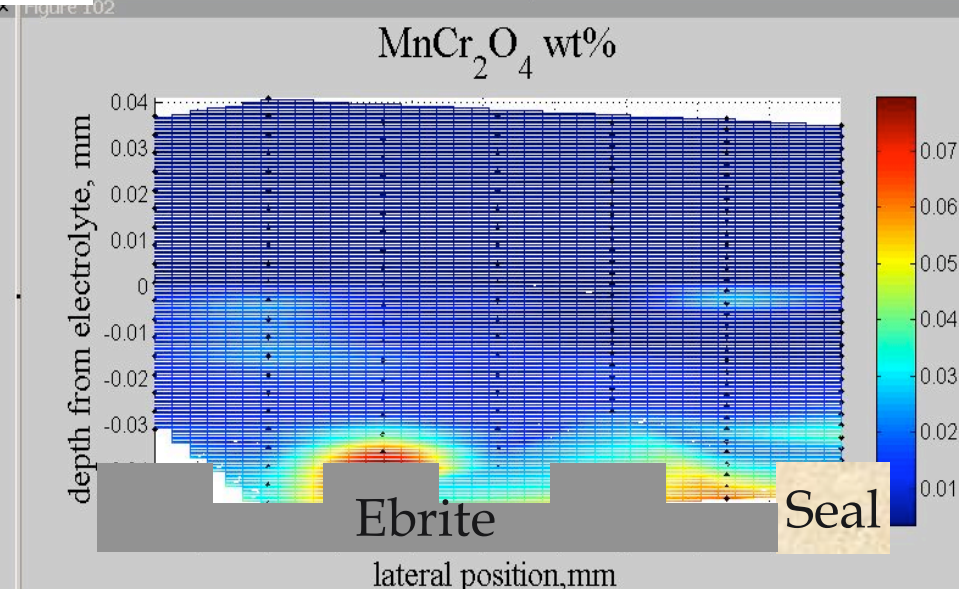
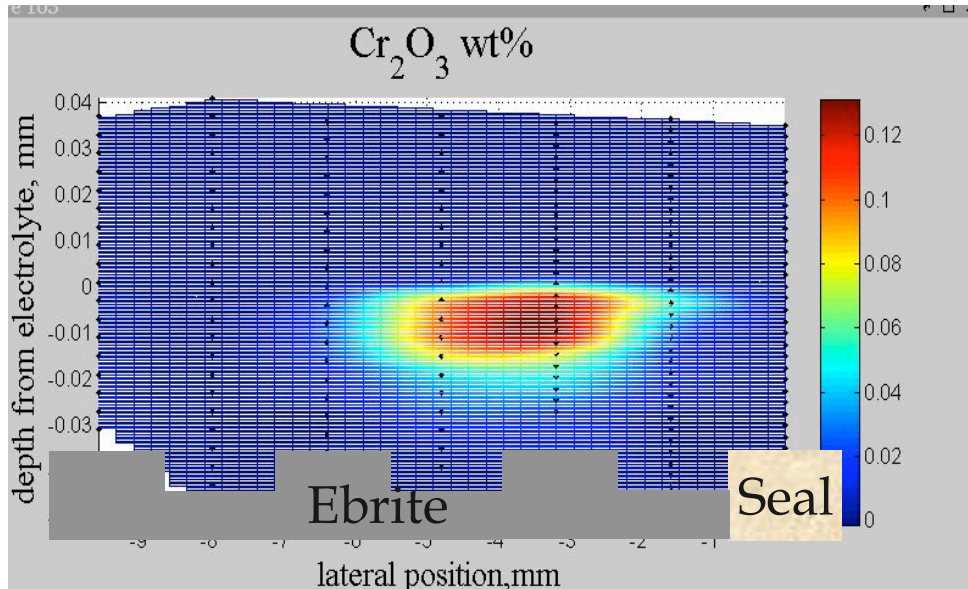
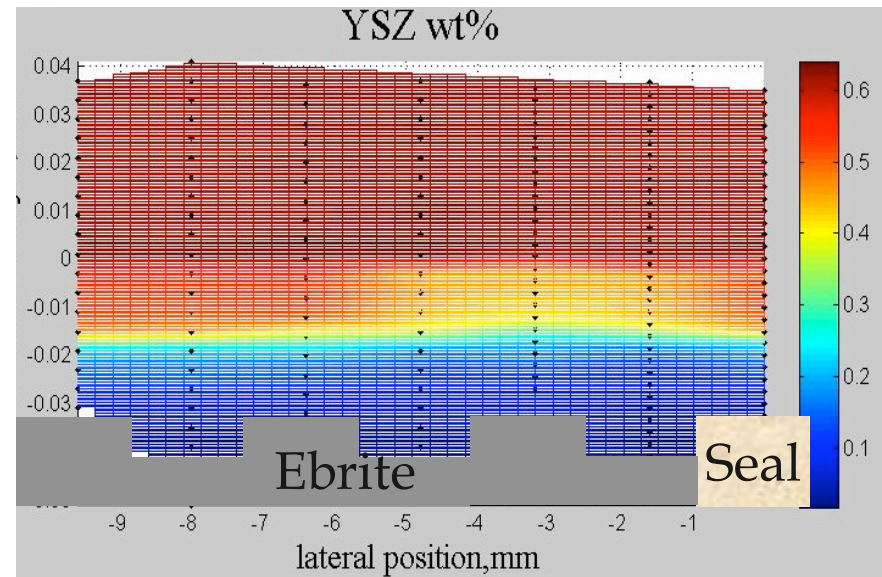
*How low can you go?*





# GSAS-derived weight fractions for 4/5 SOFC phases

- Transition between 2 Cr phases in “active cathode” region
- $\text{Cr}_2\text{O}_3$  strongly associated with YSZ content and current collector position
  - suggests formation through electrochemical reduction
- Cr/Mn spinel has weaker spatial association
  - possibly formed by direct chemical process (Cr transport through gas & solid diffusion)
- A continuous layer of  $\text{Cr}_2\text{O}_3$  built at the cathode/ electrolyte interface
  - probably plays a key role in raising impedance and blocking mass transfer



# *Cr<sub>2</sub>O<sub>3</sub> and (MnCr)<sub>3</sub>O<sub>4</sub> Phase and Concentration Distribution in Deactivated SOFC Cell*

## Cr Accumulation Mechanism

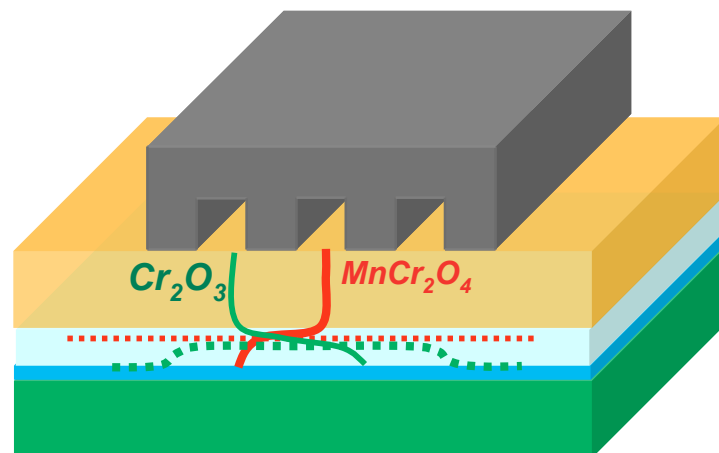
- Generation at metallic interconnect



- Deposition through Electrochemical Process



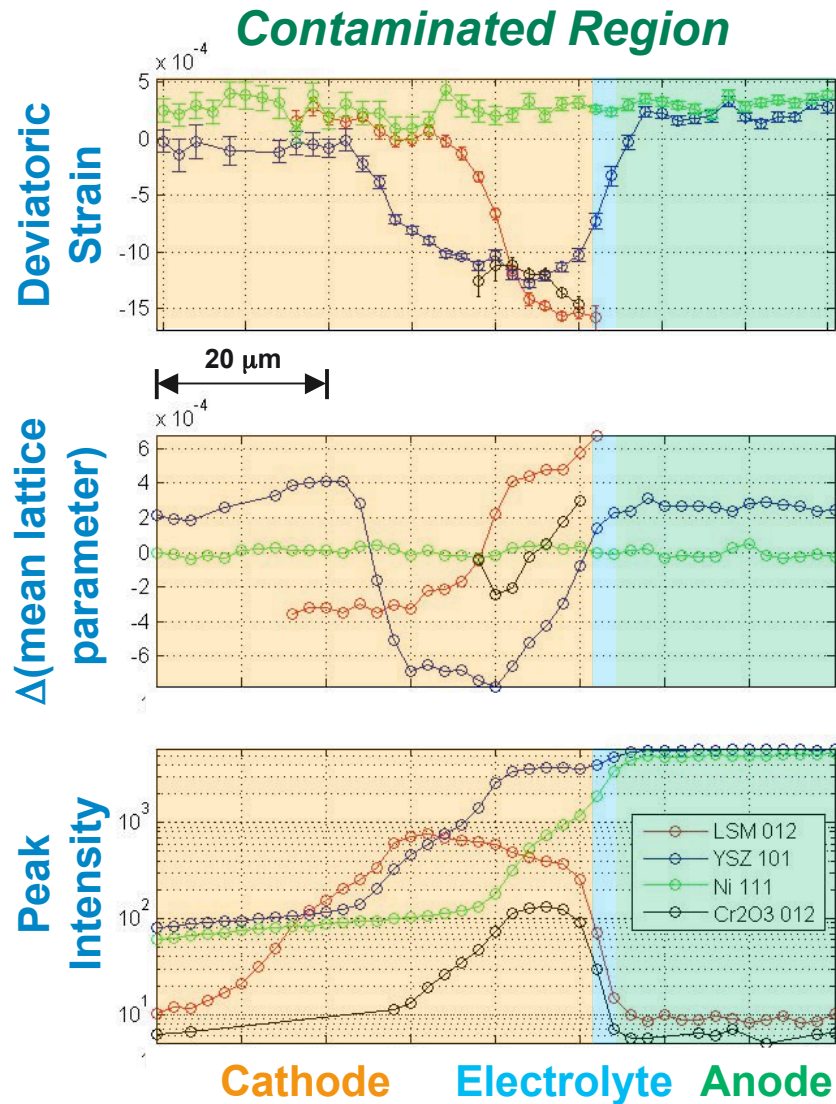
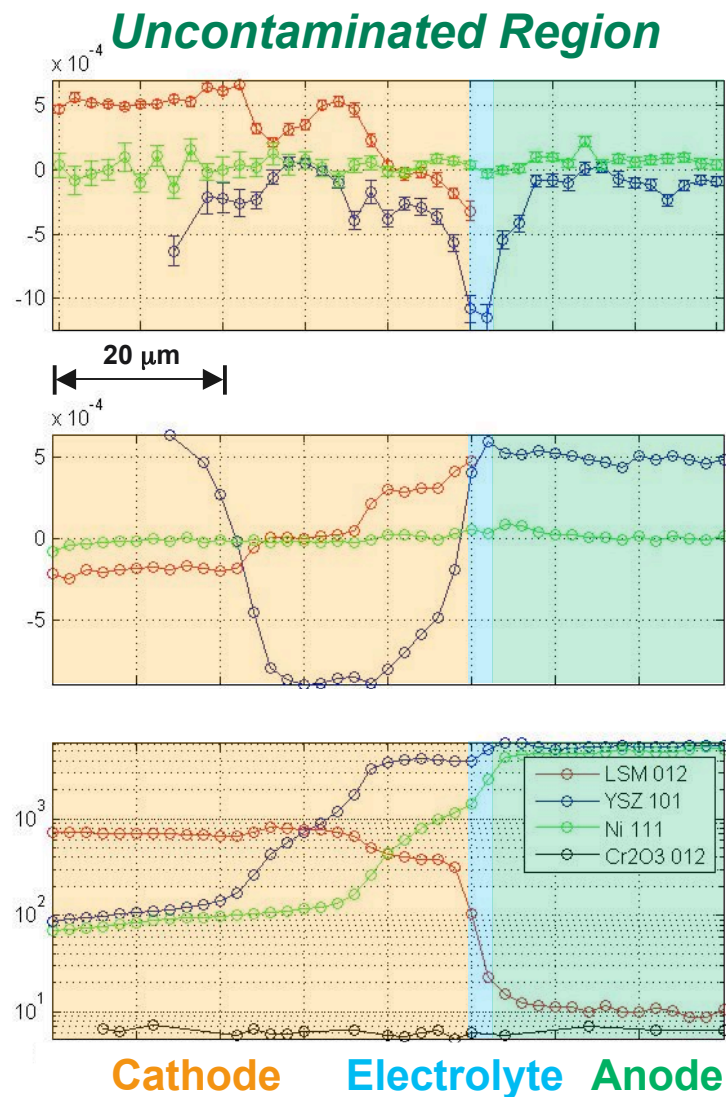
- Deposition through Chemical Process



K. Hilpert, D. Das, M. Miller, D. H. Peck and R. Weiß, *J. Electrochem. Soc.* **143**, 3642, 1996

S. P. S. Badwal, R. Deller, K. Foger, Y. Ramprakash, J. P. Zhang, *Solid State Ionics*, **99**, 297, 1997

# Internal strain and intraphase composition versus depth





# ***Case study II: Strain and stress mapping in advanced structural steels***

*Collaborators:*

*Yana Qian and Greg Olson*

*Northwestern University*



# Advanced structural steel

## Material - **Ferrium® C67**

- Belongs to a new class of carburized secondary hardening gear and bearing steels, utilizing an efficient M2C precipitate strengthening dispersion.
- Combines a tough ductile core with an ultra-hard carburized case that can achieve hardness levels of up to 67 HRC, promoting high wear and contact fatigue life.
- Is the product of an ongoing research and development program with the objective of reducing gear weight by as much as 50% over conventional carburized gear steels.

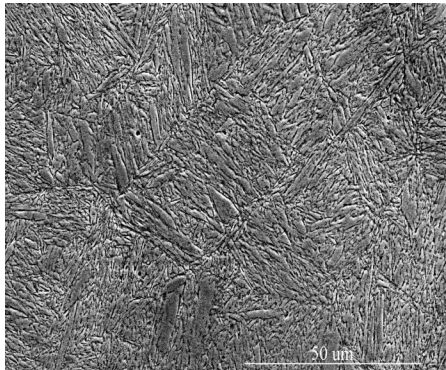
US Patent Number 6,176,946 B1

## Application

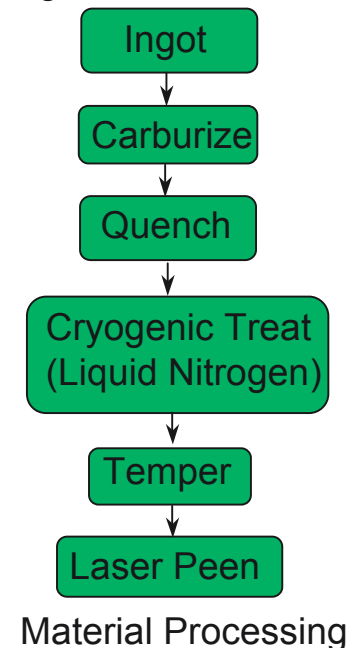
- High power density transmission systems: helicopters, heavy machinery, racing, and manufacturing.

## Material Properties

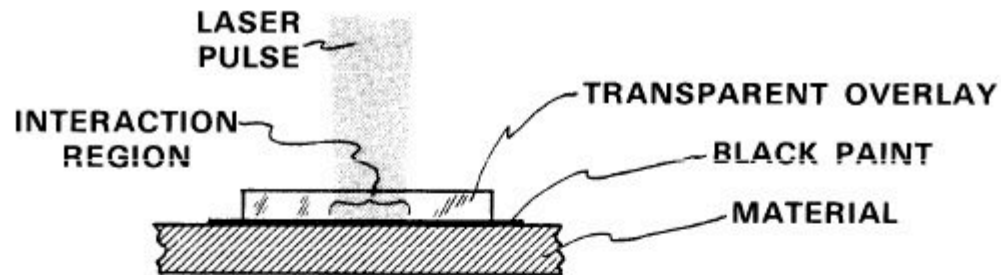
Temper	YS (ksi)	UTS (ksi)	EI (%)	Core Hardness (HRC)	Case Hardness (HRC)
Overage	180	230	17	48-50	65-67



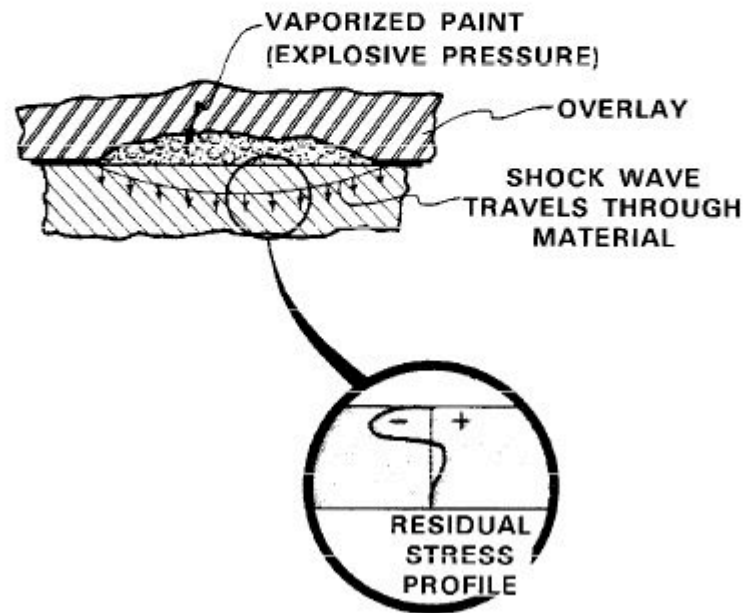
C67 microstructure (SEM)



## Laser Peening



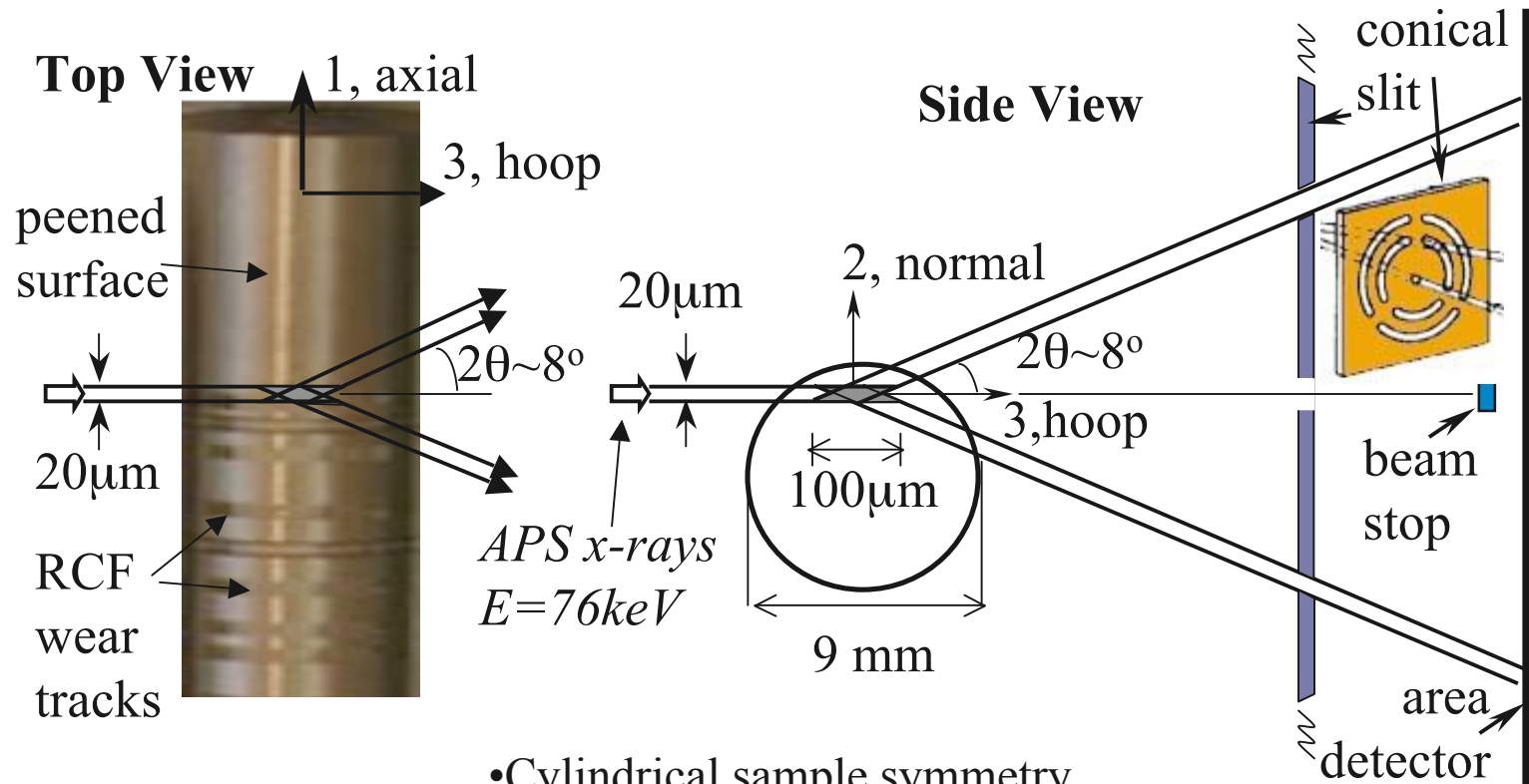
a. Surface area to be laser shocked, showing the laser beam and overlays.



b. Effect of laser beam at the overlay-workpiece interface.

Ref: Laser Shock  
Processing Technical  
Bulletin No. 1, LSP  
Technologies, Inc.

## Experimental geometry for non-destructive mapping

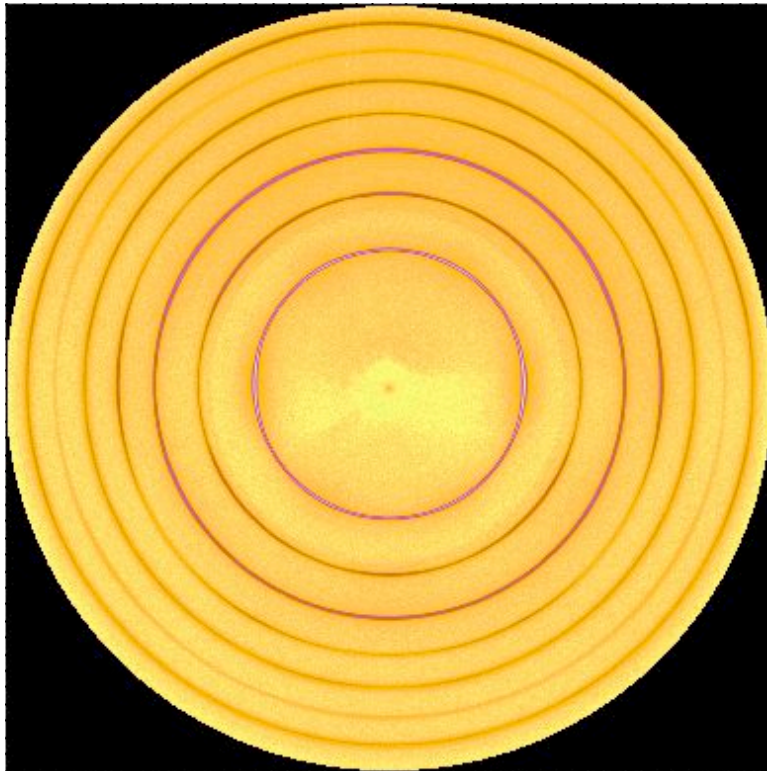


- Wear samples
- Ground
  - Shot peened
  - Laser peened

- Cylindrical sample symmetry
  - rotate for grain averaging
- Conical slit
  - 3-d gage volume ( $\sim 20 \times 20 \times 150 \text{ um}^3$ )
  - normal & axial components simultaneously
- move sample in x2 for depth resolution

## Diffraction Patterns from sample

### Without Conical Slit

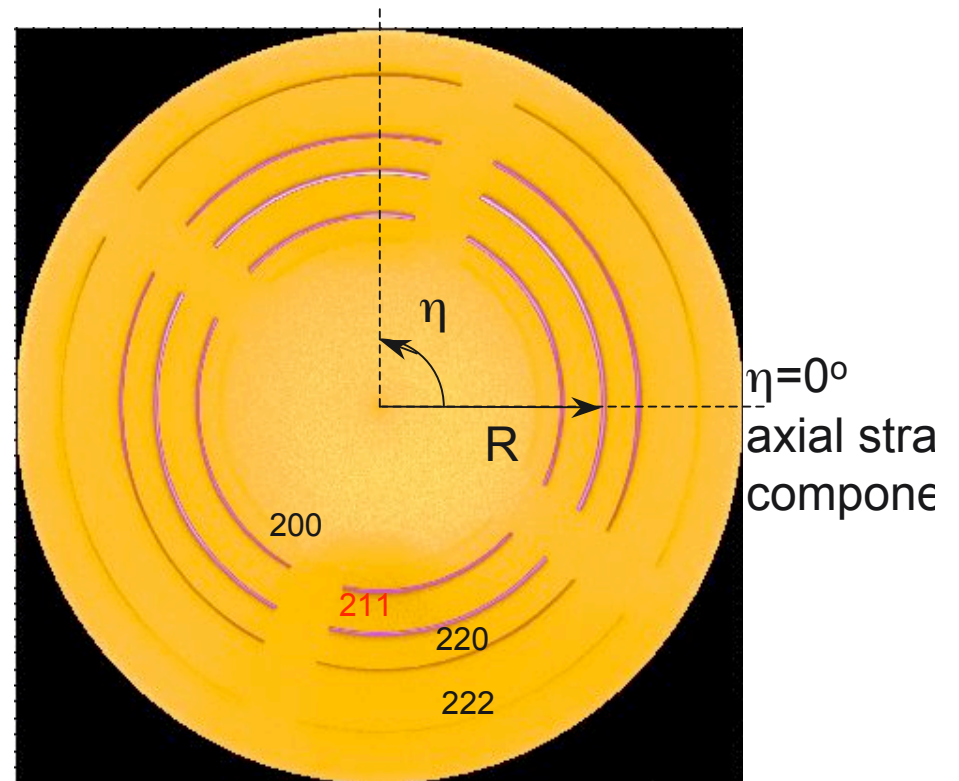


Powder Diffraction

7 BCC reflections

### With Conical Slit

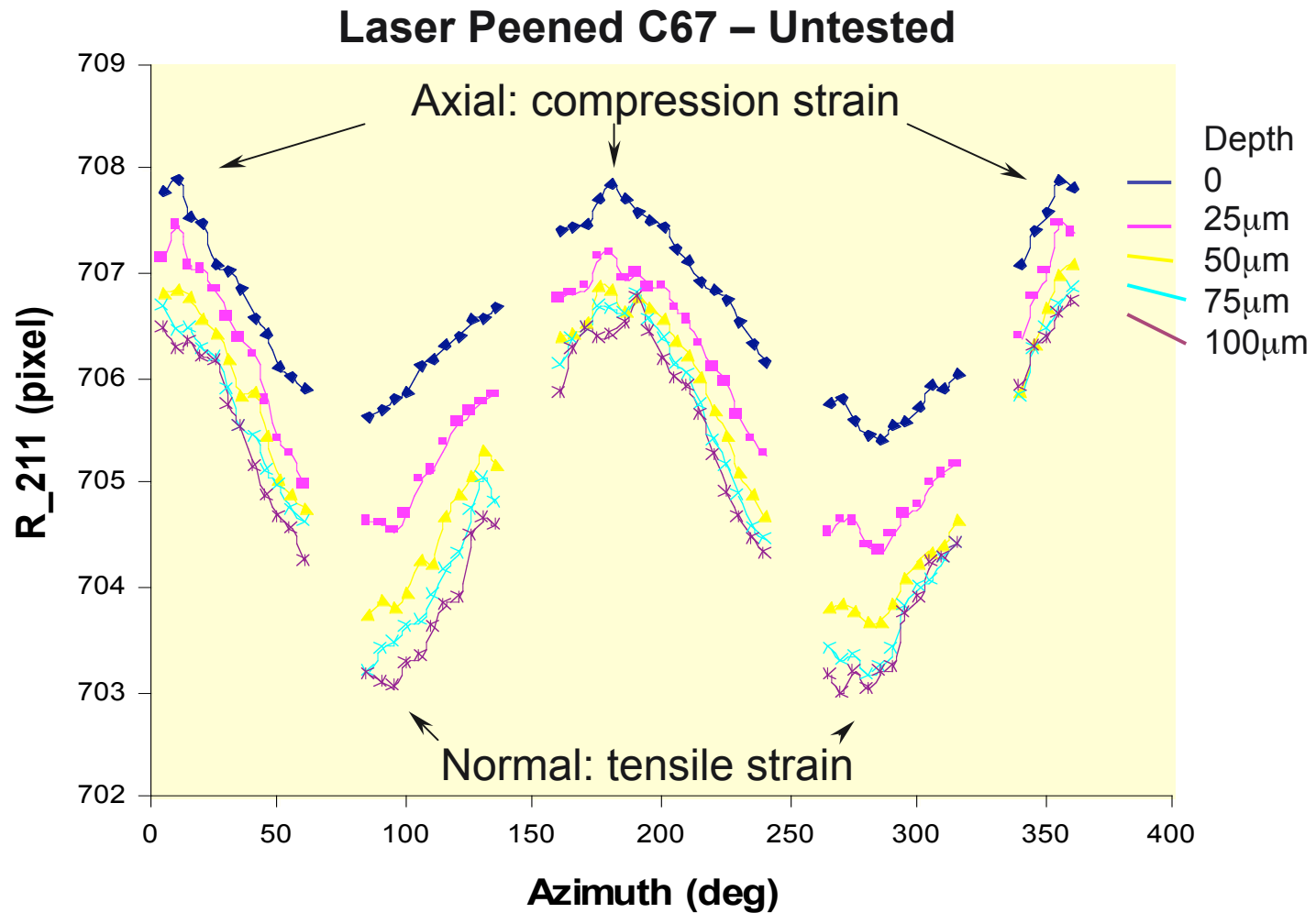
$\eta=90^\circ$  normal strain component



4 BCC Reflections

(211) is chosen for analysis.

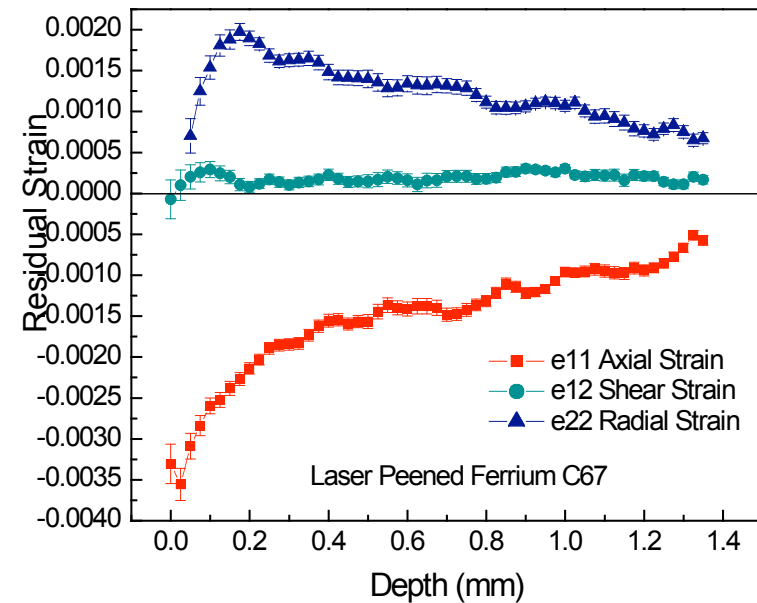
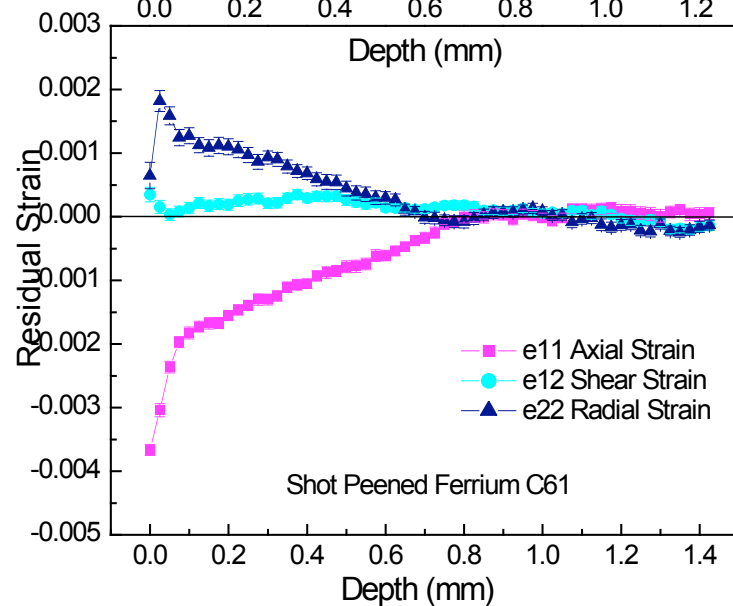
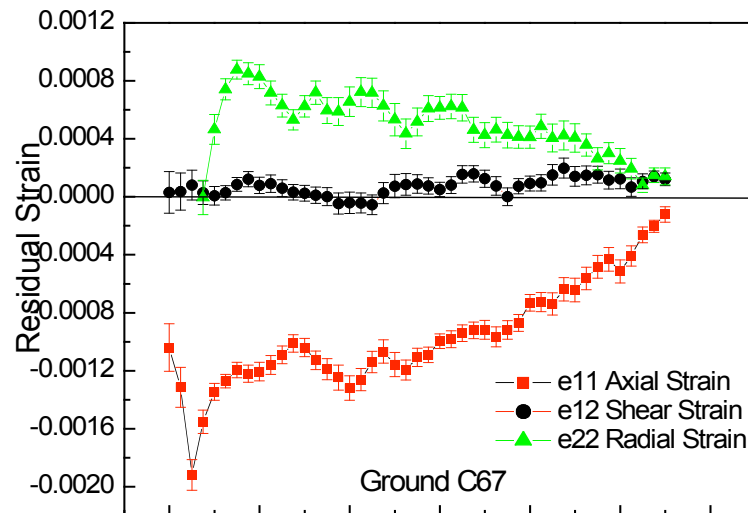
## Peak position versus orientation – deviatoric strain



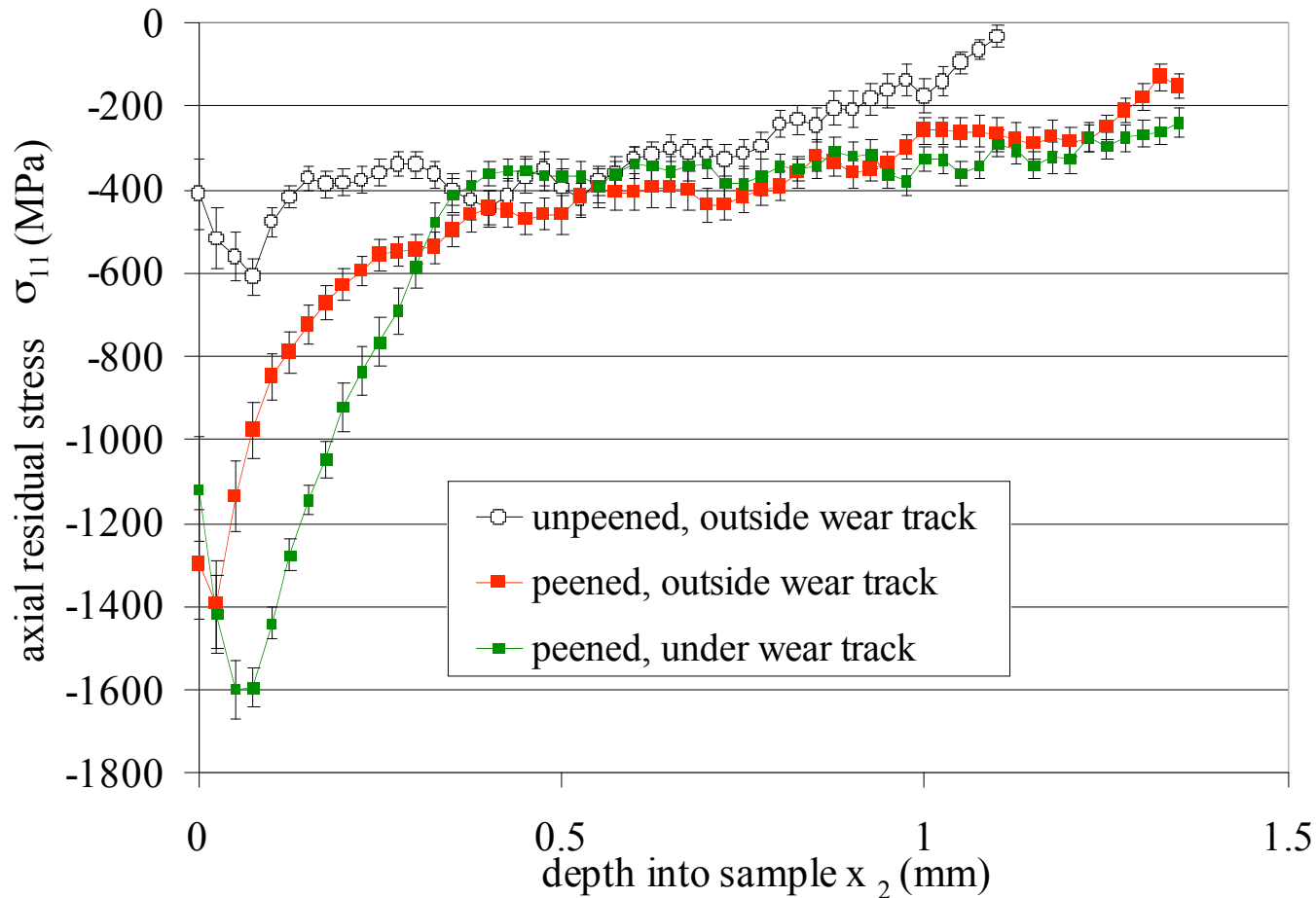


## Residual Strain vs Depth – 3 conditions

- Results for martensite (211):
- 3 measured strain components
- regions away from wear tracks
- 25  $\mu\text{m}$  step width

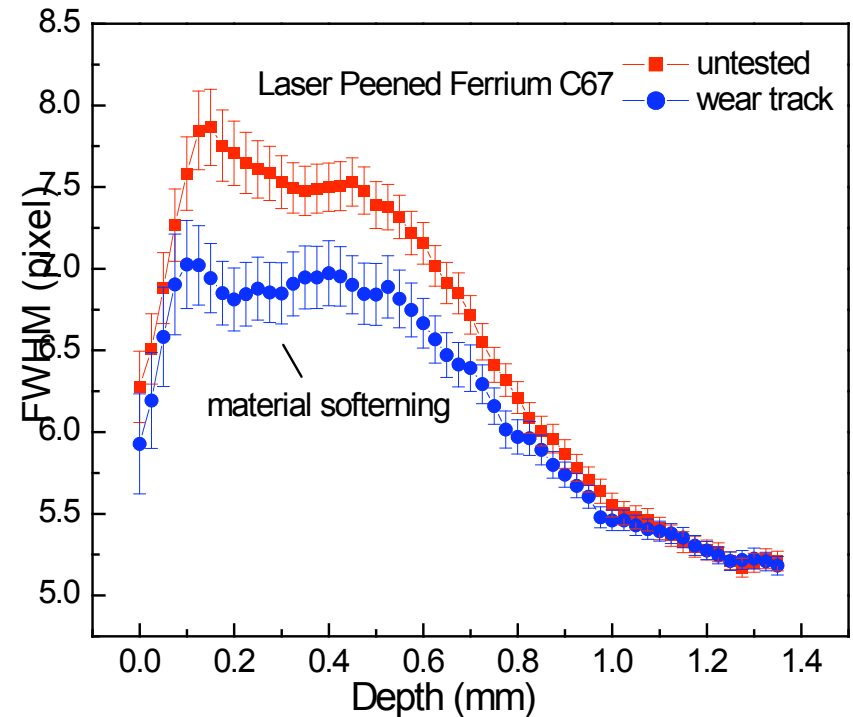
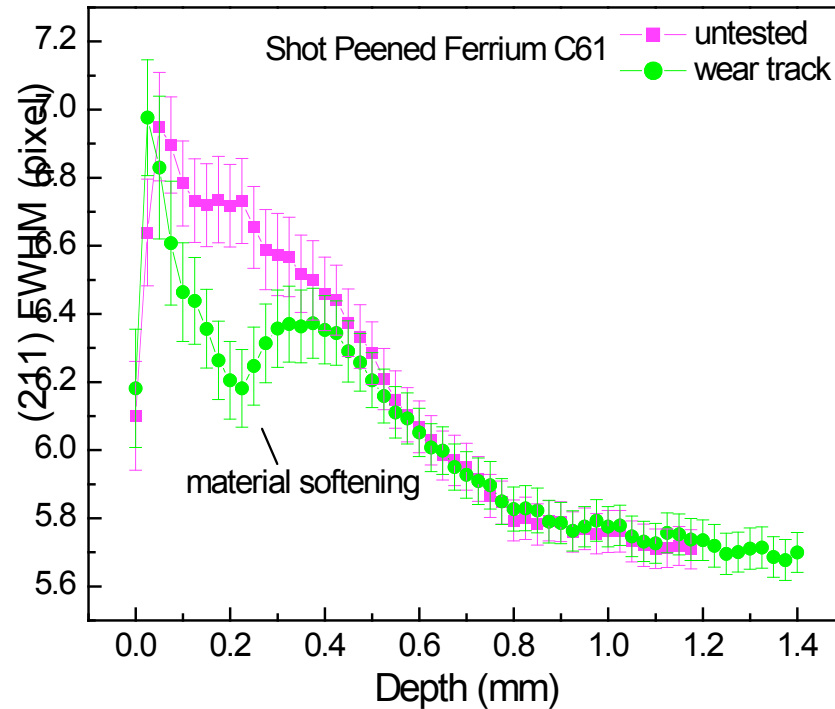


## Residual Stress vs Depth, Laser-Peened Sample



- Main observations
- Significant compressive residual stresses due to initial thermo-mechanical processing
  - Increase in RS after laser peening
  - After RCF, RS maximum shifts to subsurface, no appreciable fading

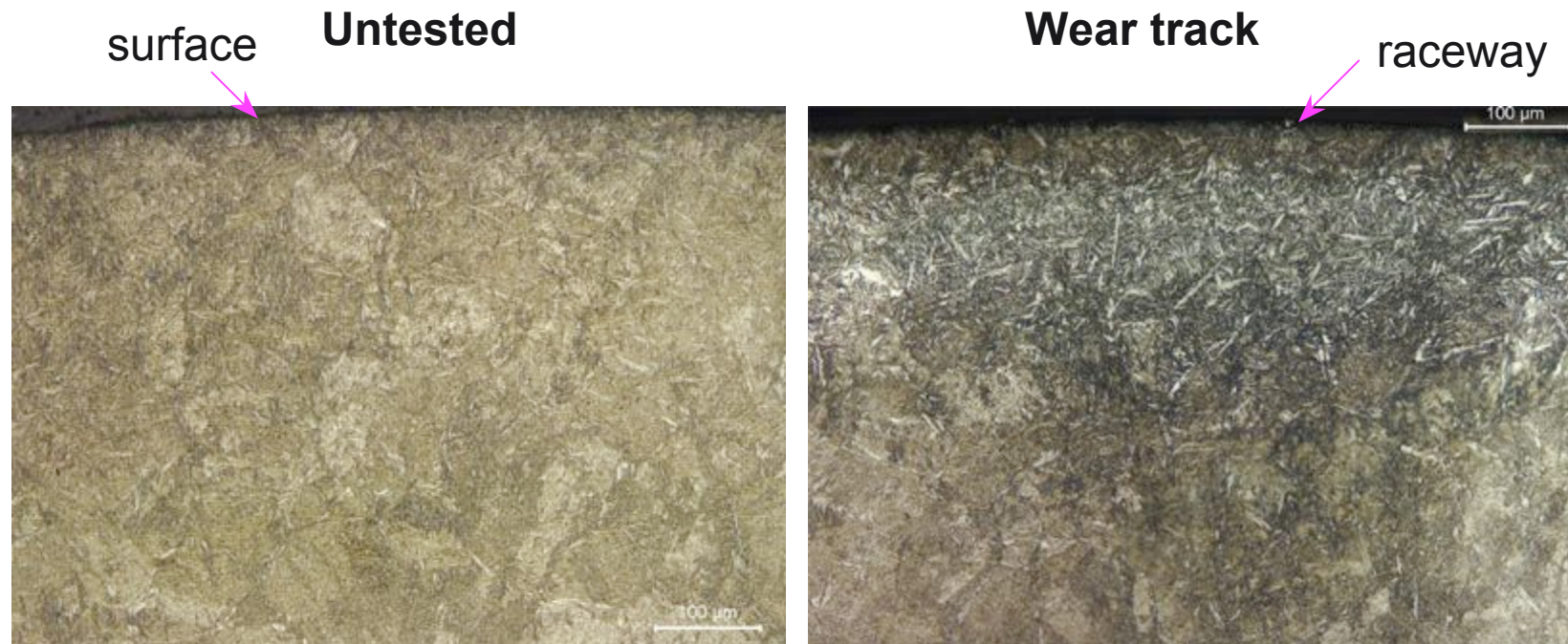
## *Additional microstructural information: peak broadening vs depth*



RCF wear induces reduction in peak broadening  
– lower martensite fraction and/or defect density

## *Confirmation of microstructural changes with optical microscopy*

Laser Peened C67 Cross Section Optical Images



Microstructure alters during rolling contact fatigue, suggesting partial transformation from martensite to ferrite.

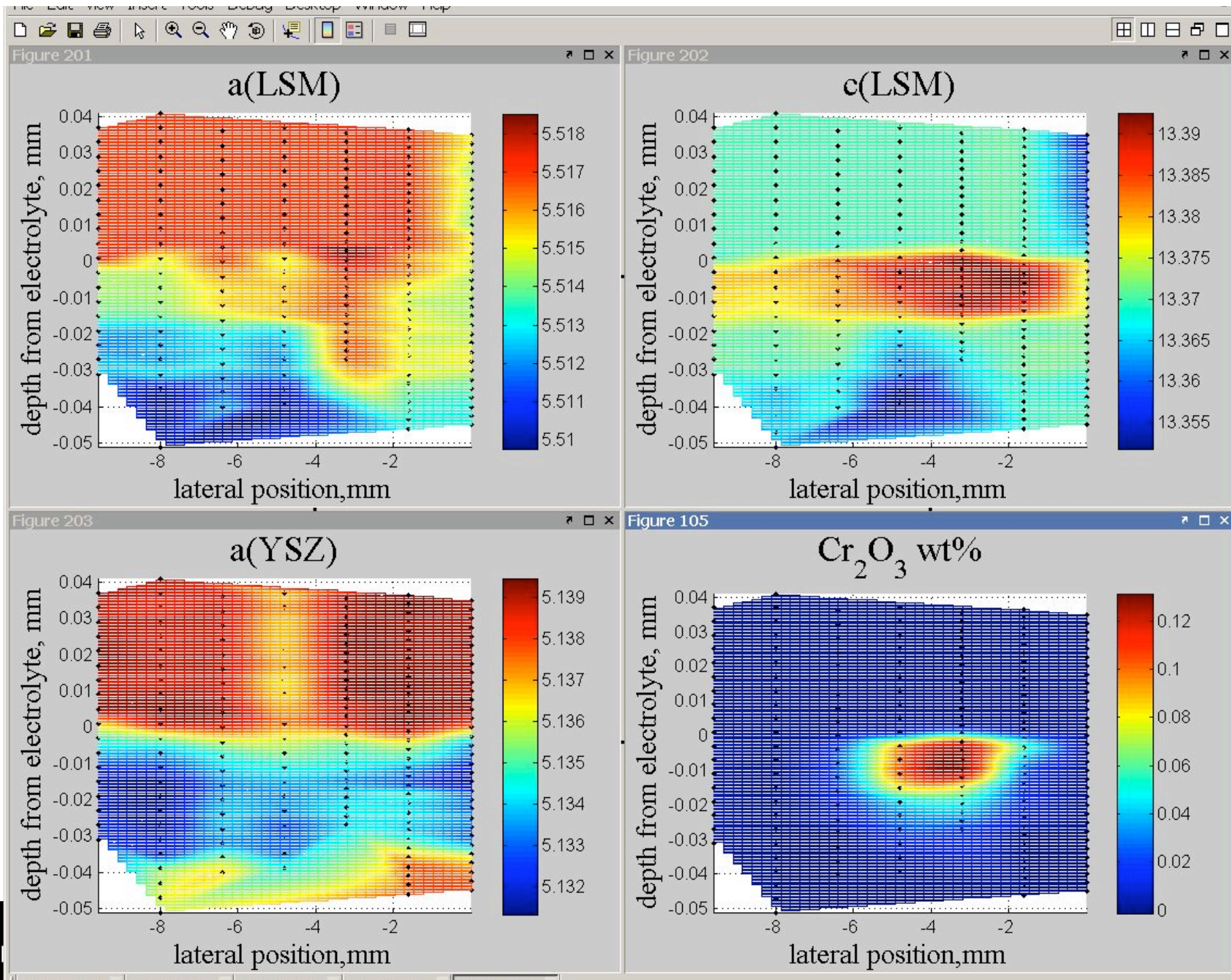
## Summary and Outlook

- High-energy x-ray scattering is a powerful technique for materials investigation
- Sector 1 instrument benefits from:
  - 7 GeV synchrotron + undulator source
  - Optics:
    - *Brilliance-preserving monochromator*
    - *Refractive focusing lenses*
    - *Conical slit*
  - Two-dimensional detectors (fast and large)
- Solid –oxide fuel cell stack
  - Gage volume  $\sim 2 \times 50 \times 1000 \text{ } \mu\text{m}^3$
  - Phase ID – yields information on mechanism of Cr-poisoning
  - Strain – TEC differences are non-negligible,  $\text{Cr}_2\text{O}_3$  induces additional strain.
  - Lattice parameter – stoichiometry variations clearly seen
  - Future *in situ* studies are envisioned
- Advanced structural steel
  - 3-d gage volume  $\sim 20 \times 20 \times 150 \text{ } \mu\text{m}^3$
  - High residual stresses due to laser and shot-peening
  - Stress relaxation under wear tracks

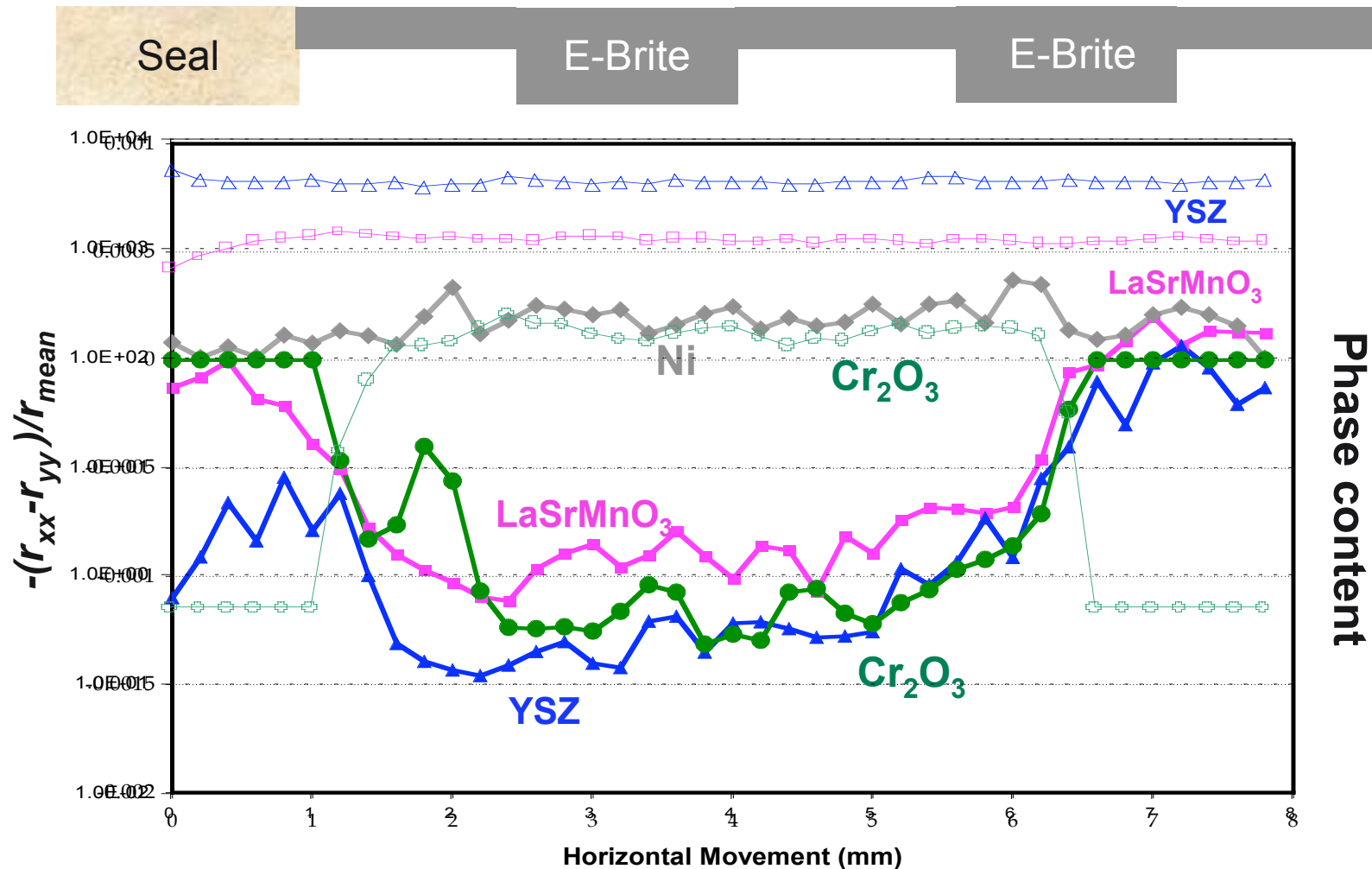
## ***Potential New Applications of Microfocused X-ray Scattering Technique for the Study of SOFCs***

- New phase identification at different boundary and depth of layers
- Solid state interfacial reaction between different phases
- 3-D strain and lattice deficiency distribution
- Density, surface area, porosity, grain size and morphology changes in SOFC at micron spatial resolution
- *In-situ*, real-time study at elevated temperature (1000 °C, 50~100 °C/sec)
- *In-situ*, real-time study under SOFC operating conditions





# Accumulation of $\text{Cr}_2\text{O}_3$ Induces Deviatoric Strains on All Phases



In-plane compressive strains are directly associated with  $\text{Cr}_2\text{O}_3$  buildup

## Distribution of Different Cr Phases as a Function of Cathode Depth

